

TOPICS

- * TF, BD, SFG \rightarrow 1m or 2m
- * TDA
 - Transient Analysis
 - Steady State Analysis
- * S \rightarrow Time domain tech \Rightarrow RH/RL
 - frequency domain tech \Rightarrow BP/NP.
- * Compensators / controllers
- * State Space Analysis \rightarrow 2m
- Subject:
- \Rightarrow TF \Rightarrow mathematical equivalent model for the s-domain.
- $$TF = \frac{1}{s+1}$$
 order - 1.
- Order represents the no. of energy storage elements (or) No. of time constants
- * Single time constants elemts are RL, RC.
- * Control sfrm's are basically LPF.

$$v_i(s) \quad \frac{1}{sC} v_o(s) \quad \frac{v_o}{v_i} = \frac{1}{sRC + 1} = \frac{1}{sT + 1}$$

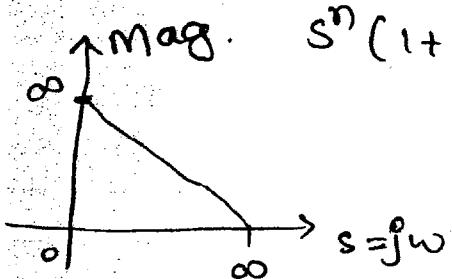
- * main objective of control sfrm is Desired output (or) accurate op.
- \downarrow
NOISE \Rightarrow should not be there.
- \downarrow
~~un. freq. high frequency.~~

Adv. of LFT:

NOISE \Rightarrow can be eliminated by LPF. at high freq
 \Rightarrow values of different components are more stable.

→ At low frequency, components are more stable.
The standard form of shm is represented as

$$shm = \frac{K(1+s\tau_1)(1+s\tau_2)(1+s\tau_3) \dots}{s^n(1+s\tau_a)(1+s\tau_b)(1+s\tau_c) \dots}$$



$P > Z \Rightarrow$ LPF (there should not be zero at strictly proper origin).

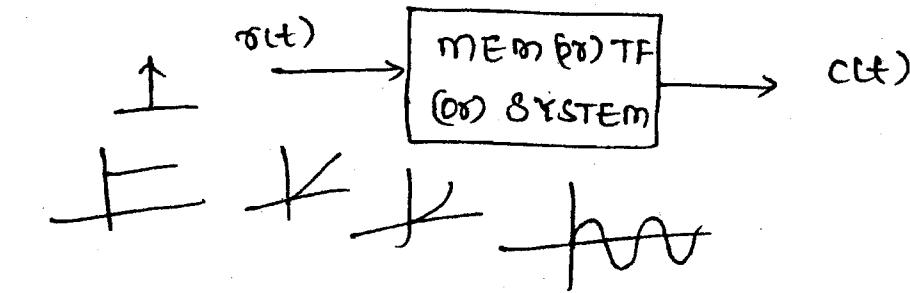
Transfer fn.

$P = Z \Rightarrow$ LP | HP | All pass | BP | BS \Rightarrow proper T.F

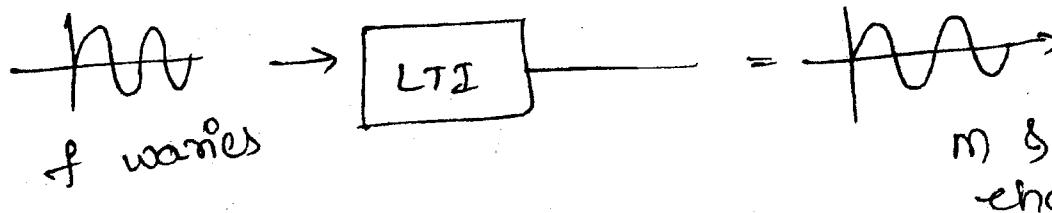
$P < Z \Rightarrow$ Nonproper Transfer function

* To find overall T.F of a big shm's like industry's, BD, SFD are used.

TDA:



very large then slow response
(t_d, t_r, t_p, t_i)
 $\%_{mp}, C_{ss} \rightarrow$ less accurate
 \rightarrow less relative stable & more oscillations.



$m \& k$ changes.

* TO evaluate shm performance w.r.t. to time
 \Rightarrow TDA

control sys specification: smallest t_r, t_s .

\Rightarrow TDA Speed $\Rightarrow t_r, t_s \downarrow \downarrow \downarrow$ quick response
v. less

2) Accuracy \Rightarrow $\epsilon_{es} \downarrow \downarrow$ (very small) \Rightarrow more accurate

3) Stability \Rightarrow $G_m \& P_m$

FDA when both very large \rightarrow (adr) More Relative stable.
 $(D_F - adr) \downarrow \downarrow$, But slow response.

Optimum ranges

5dB to 10dB $\rightarrow G_m$

80° to $40^\circ \rightarrow P_m$.

When both very less \rightarrow (adv) Less relative stable
 $(D_F - adv) \downarrow \downarrow$, More oscillator.

4) Sensitivity w.r.t. Noise, Disturbance, environment condition (Temperature) etc. $t_S \downarrow \downarrow t_g \uparrow \uparrow$

The best sys is insensitivity w.r.t. N, D, Etc Etc

* Transient performance is improved means \Rightarrow speed of the performance improved.

steady state " \Rightarrow accuracy improved

stability: stability for

* To find the closed loop sys only.

OL sys

\downarrow \downarrow \rightarrow CLTF

$G(s)$

\downarrow \downarrow OLTF of a
sys

$G(s), H(s) = 1$

\downarrow \downarrow OLTF of unity feedback sys.

$$CLTF = \frac{G(s)}{1 + G(s)}$$

CLTF

$$CLTF = \frac{C}{R} = \frac{G(s)}{1 + G(s)H(s)}$$

$G(s)H(s) \Rightarrow$ OLTF of a Non-unity fb shw

CL shw

$$OLTF \Rightarrow \text{of a shw} \Rightarrow G(s) = \frac{s+1}{s^2(s+2)(s+3)}$$

poles locations are identified directly \Rightarrow stability

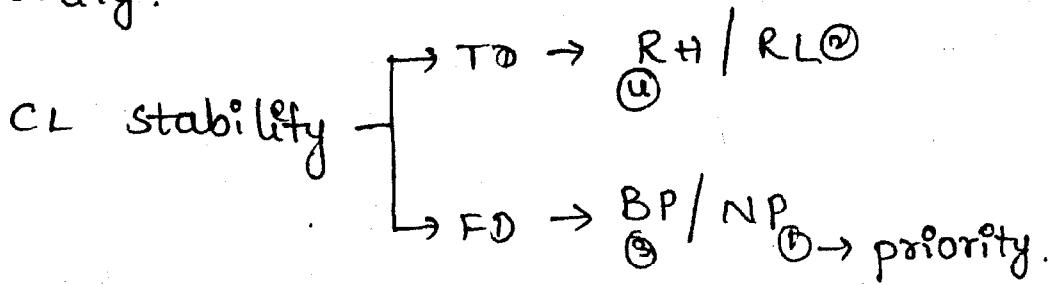
is identified \Rightarrow stability tech. is not required.

CL shw: OLTF of a unity fb shw

$$G(s) = \frac{s+1}{s^2(s+2)(s+3)} \Rightarrow CLTF = \frac{s+1}{s^2(s+2)(s+3) + s+1}$$

CL poles locations are not identified directly hence required a stability technique to find CL stable.

The feedback changes the location of poles as order increases finding the new location of the poles is very difficult. Hence we required a stability technique to find the closed loop stability.



* According to analysis TDA is best.

* Time Domain tech. gives the transient, ss.

* Freq " " " Steady state Analysis

* stability analysis is a steady state analysis.

Transportation delay / lag s/m's.

$$L\{g(t-T)\} = e^{-sT}$$

$$\text{TD: } \bar{e}^{-sT} = 1 - sT + \frac{(sT)^2}{2!} + \dots + \infty$$

Neglect-

$$= 1 - sT$$

f₀: BP: $\begin{array}{c} M \\ \uparrow \\ \omega \end{array} \rightarrow \omega$

$$\begin{array}{c} \phi \\ \uparrow \\ \omega \end{array} \rightarrow \omega$$

NP: $\begin{array}{c} M \\ \uparrow \\ \phi \end{array} \rightarrow \phi$

$$+e^{j\theta} = \cos\theta + j\sin\theta$$

$$-e^{-sT} = -e^{j\omega T} \Rightarrow m=1$$

$$\phi = (-\omega T)$$

Bode plot are drawn only for minimum phase s/m.

- ① Adv. NP:
- ① No. of CLP Right hand side
 - ② Range of K (Gain)
 - ③ Relative stability. (RS)
 - ④ PM & GM

② Adv: Root loci:

→ Nature of the s/m is identified.

- ③ BP:
- GM & PM
 - RS.

- ④ RH:
- Location of poles. Identified.